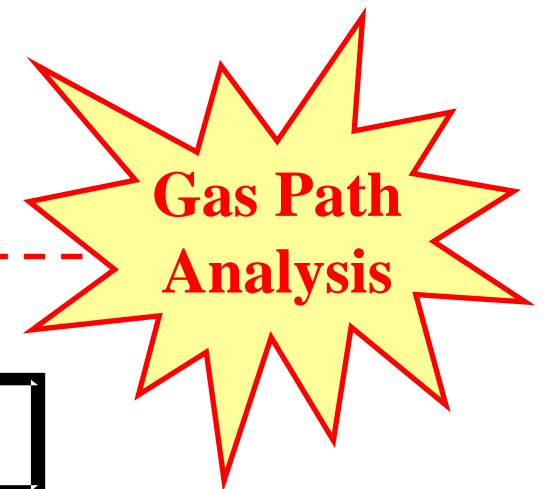
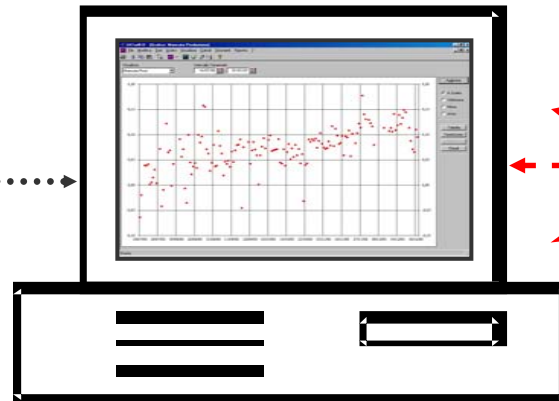
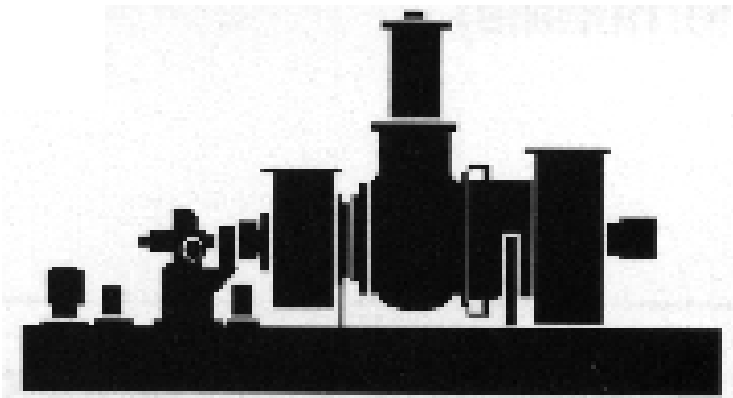


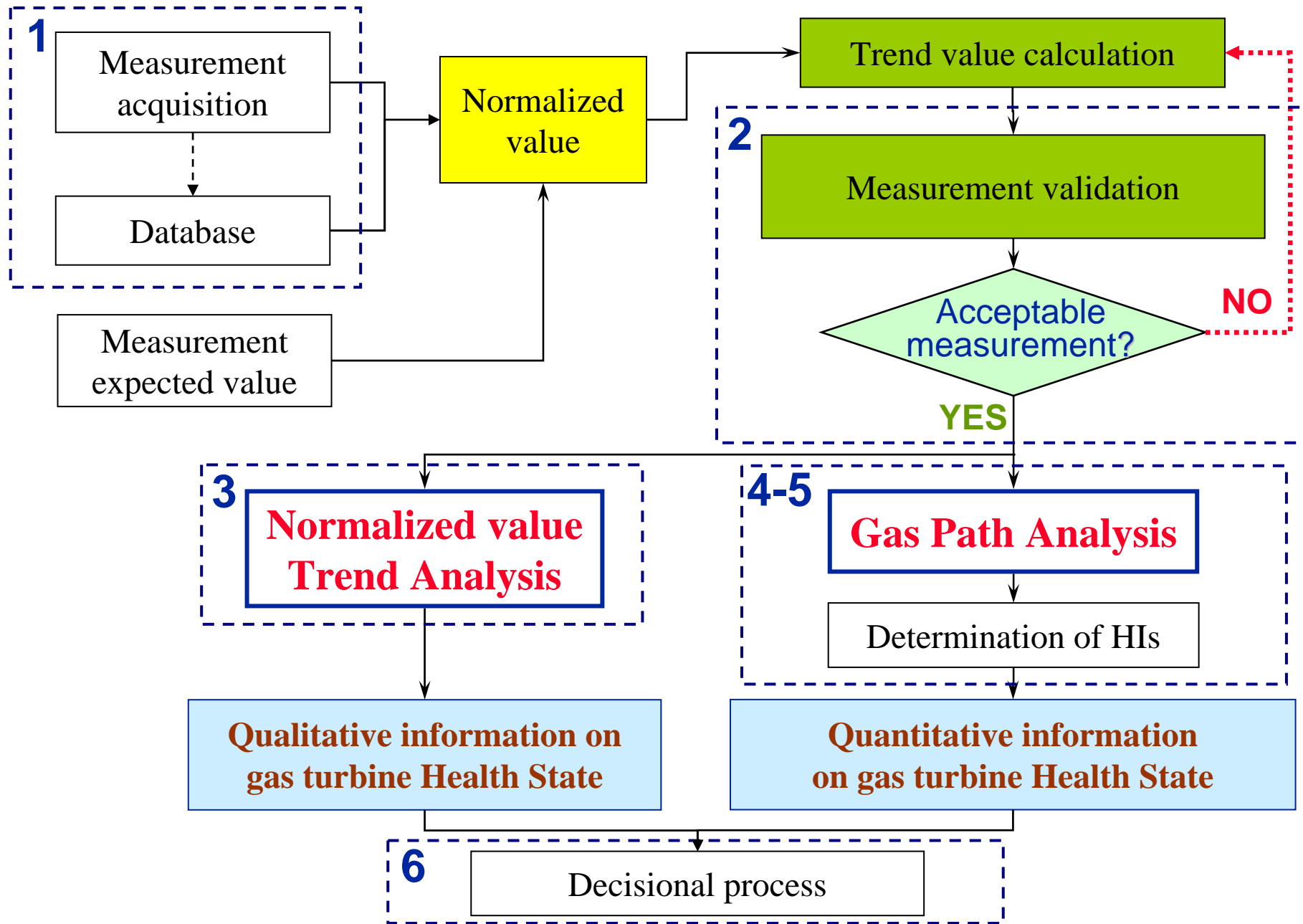
Analisi dello stato di funzionamento di turbine a gas

Gas turbine operation optimization

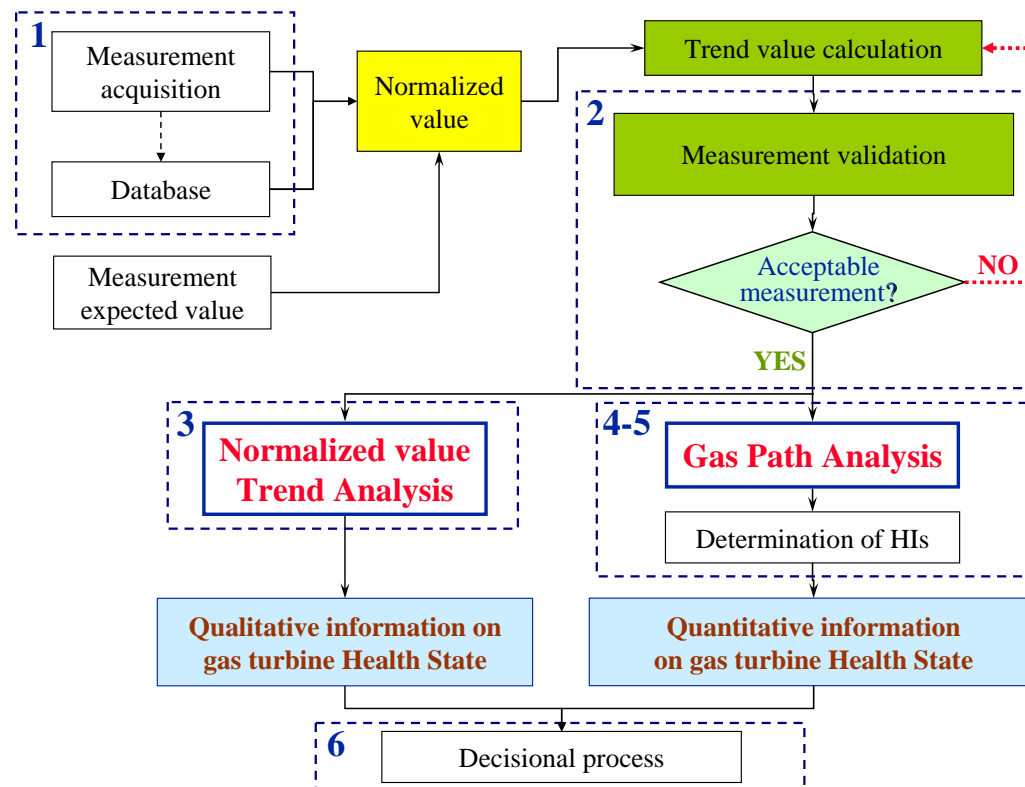
GT on-condition maintenance

Maintenance costs ↓
Management costs ↓ (Non-scheduled stops ↓)
Process interruption ↓ (Availability ↑)





The diagnostic process



✓ **Field measurements**

✓ **Thermodynamic Cycle Program**

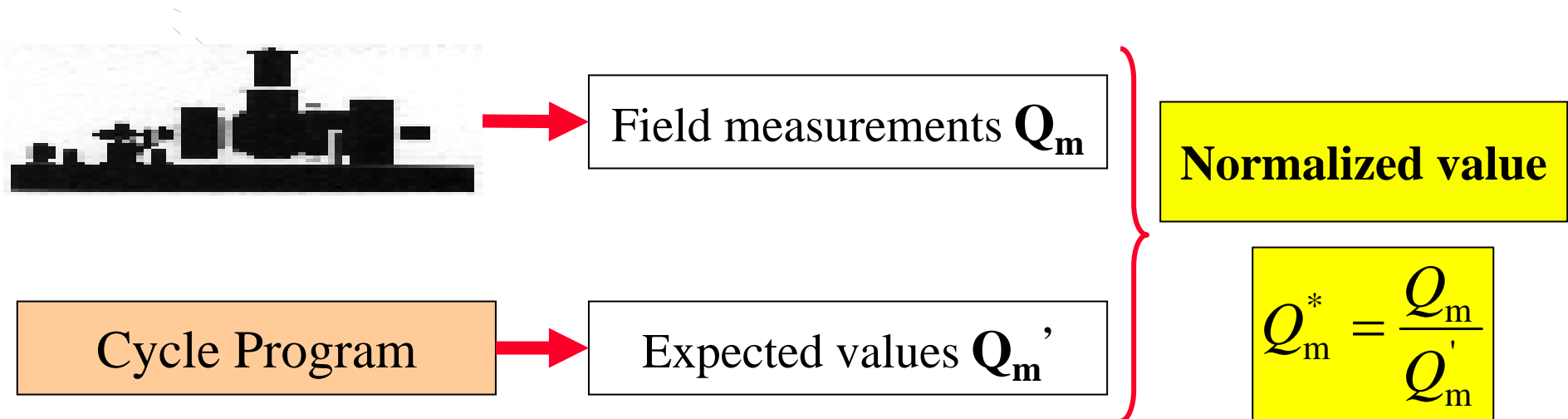
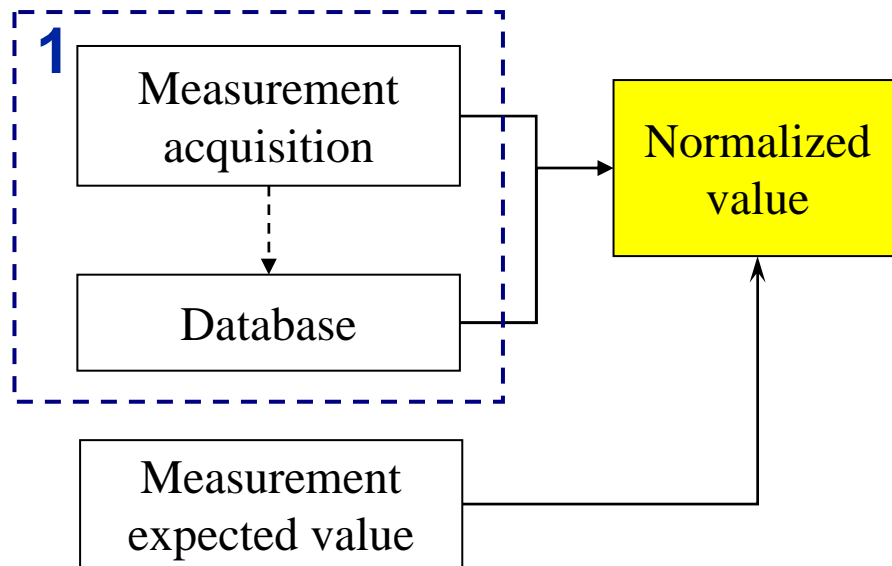
✓ **Health Indices**

✗ **Measurement accuracy**

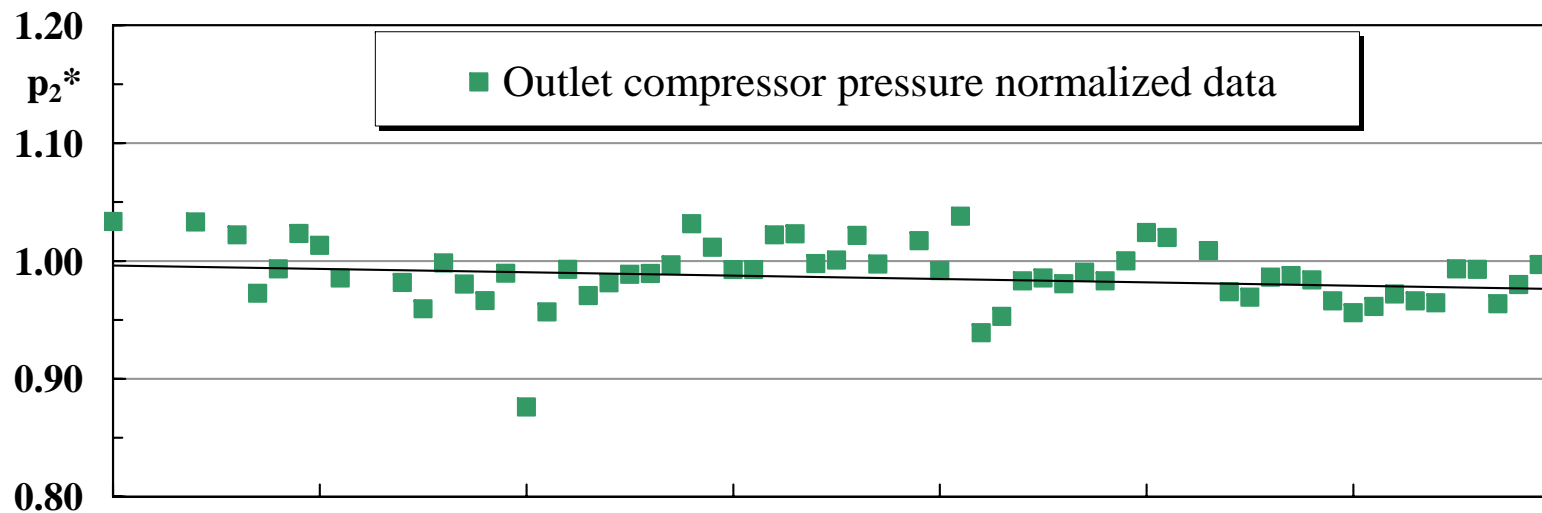
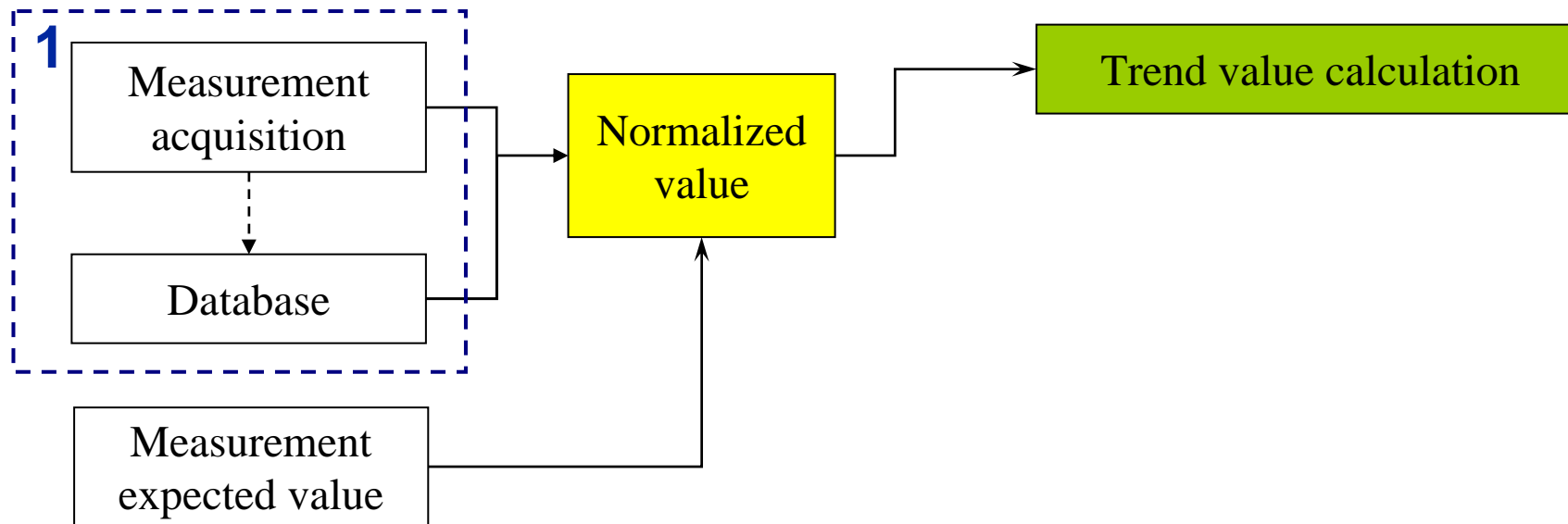
✗ **CP tuning**

✗ **Measurement number**

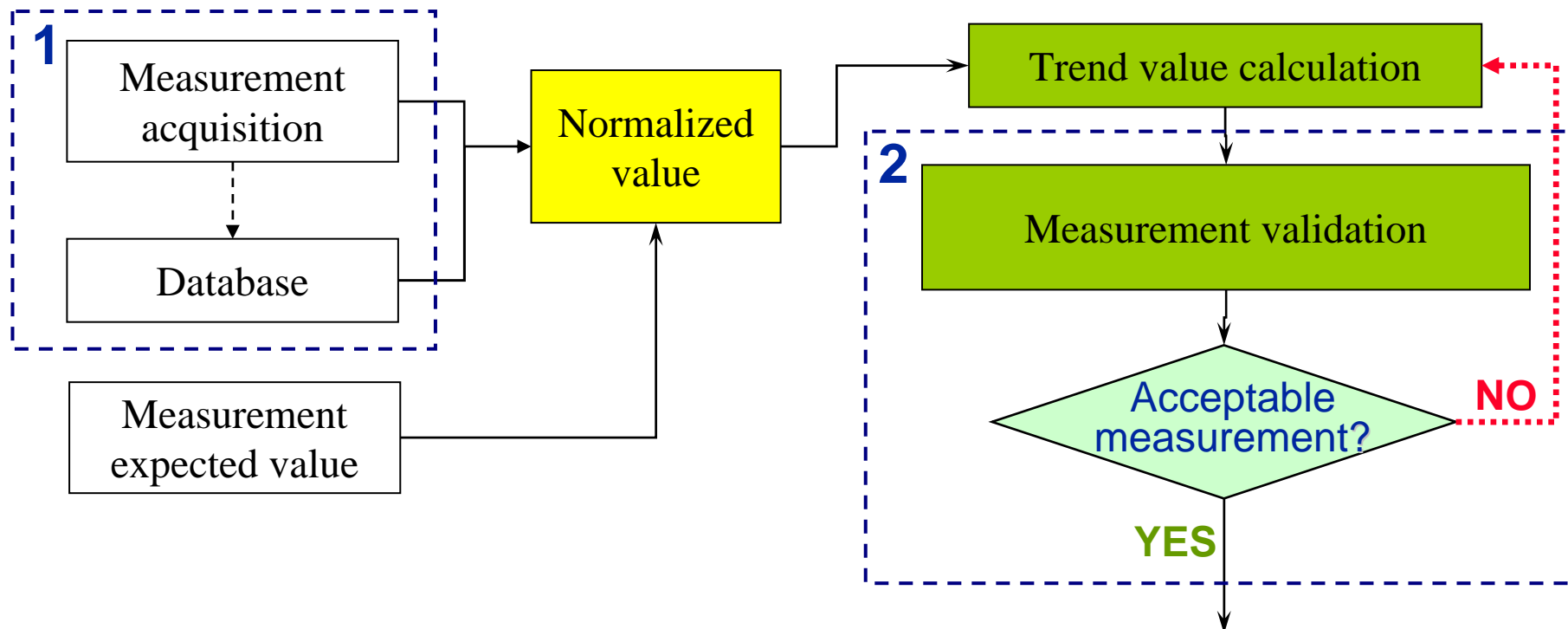
The diagnostic process (1/4)



The diagnostic process (2/4)



The diagnostic process (3/4)



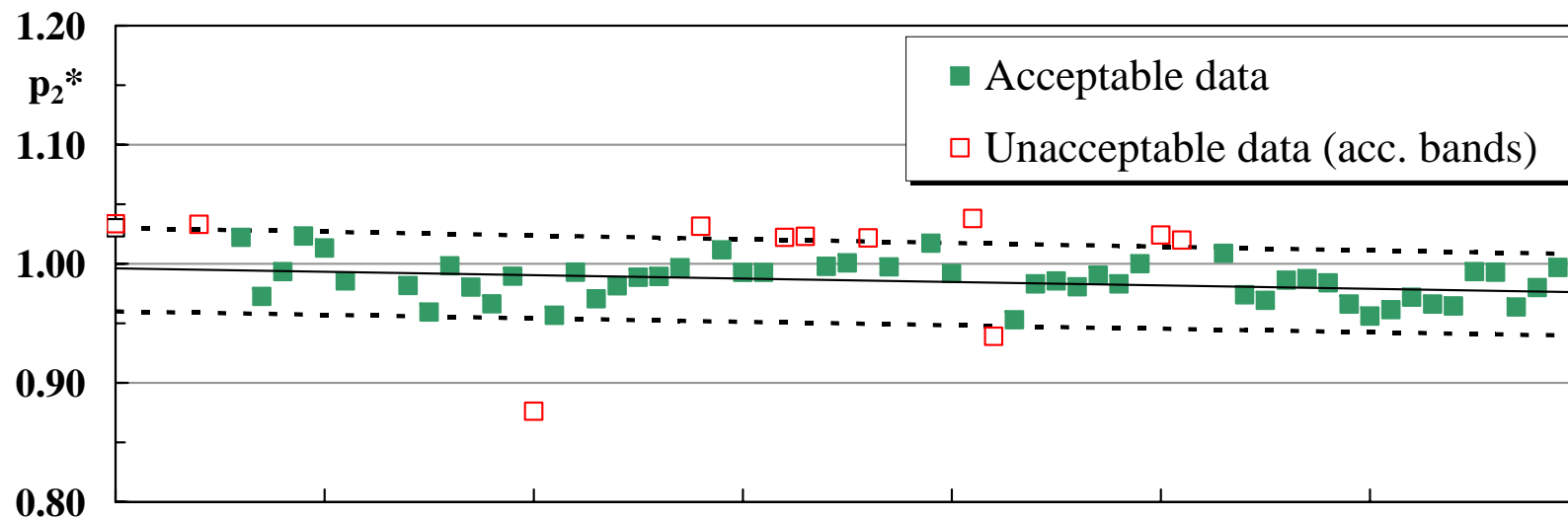
Two techniques
both applied to the
normalized trend over time
of each measurement

- ✓ **Measurement acceptability bands**, which consider
(1) meas. accuracy + acquisition system noise,
(2) engine faults and (3) CP tuning accuracy
- ✓ **Statistical technique for outlier detection** through
a test criterion, i.e. analysis of the statistical
distribution of the normalized measurement trend

Measurement validation through acceptability bands

Band amplitude: measurements accuracy and total band amplitude

Measured Quantities	Measurements accuracy [% of reference value]	Confidence band [% of trend value]
T_2	± 0.85	[-1 ; + 5.5]
p_2	± 1.00	[-4; + 3]
T_6	± 0.75	[-1 ; + 5.5]



Measurement validation through statistical techniques

$$\frac{|x_i - x_m|}{S} \geq k, \quad i = 1, \dots, N$$

- Practical and easy-to-use
- Robust

x_m = mean of the sample (N = sample size)

S = standard deviation

k = threshold, which depends on sample size N and on the level of significance α

α = probability of rejecting a good point (usually $< 5\%$)

If the inequality applies, x_i is an outlier.

- Available methods in literature: Thompson method, Grubbs method, Chauvenet criterion, ...
- These methods proved only partially effective for GT data (in fact, trends are usually not constant over time)
- Thus, a new method was developed by the authors

Statistical technique developed by the authors

$$\frac{|x_i - x_m|}{k_B S} \geq t_\alpha k_A, \quad i = 1, \dots, N$$

➤ The new coefficients account for the behavior-in-time of each quantity

$$k_A = 1 + \frac{\lim_{N \rightarrow \infty} t_\alpha^2 + 1}{4N}$$

➤ k_A tends to one when N tends to infinity

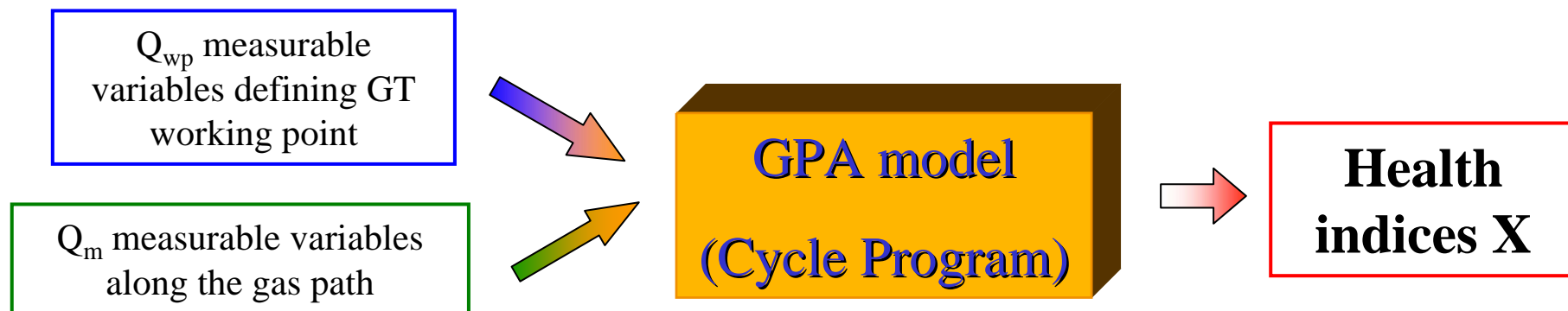
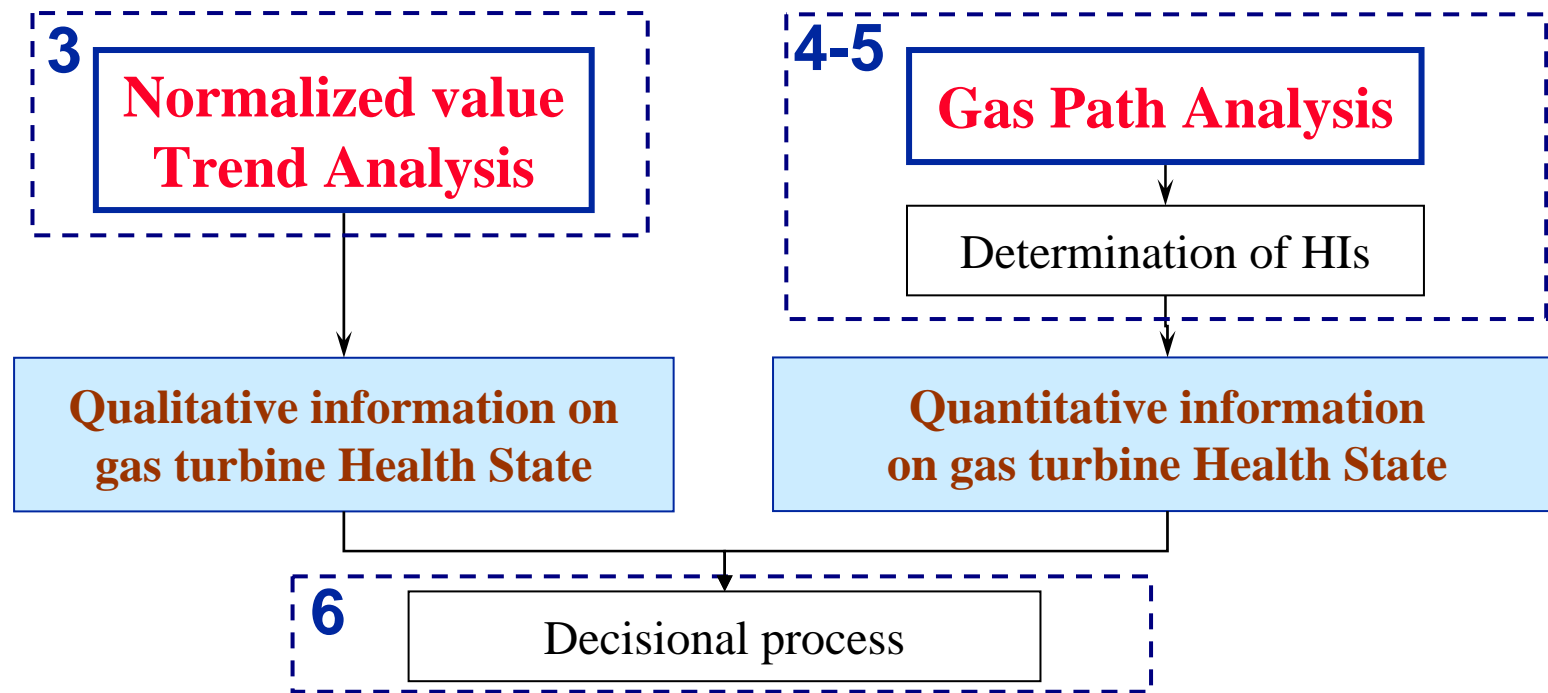
➤ t_α represents the value of the quantile corresponding to a certain level of significance

$$k_B = (1 + N)^{\frac{1}{N}} (1 + |S_{ov} - S_i|)$$

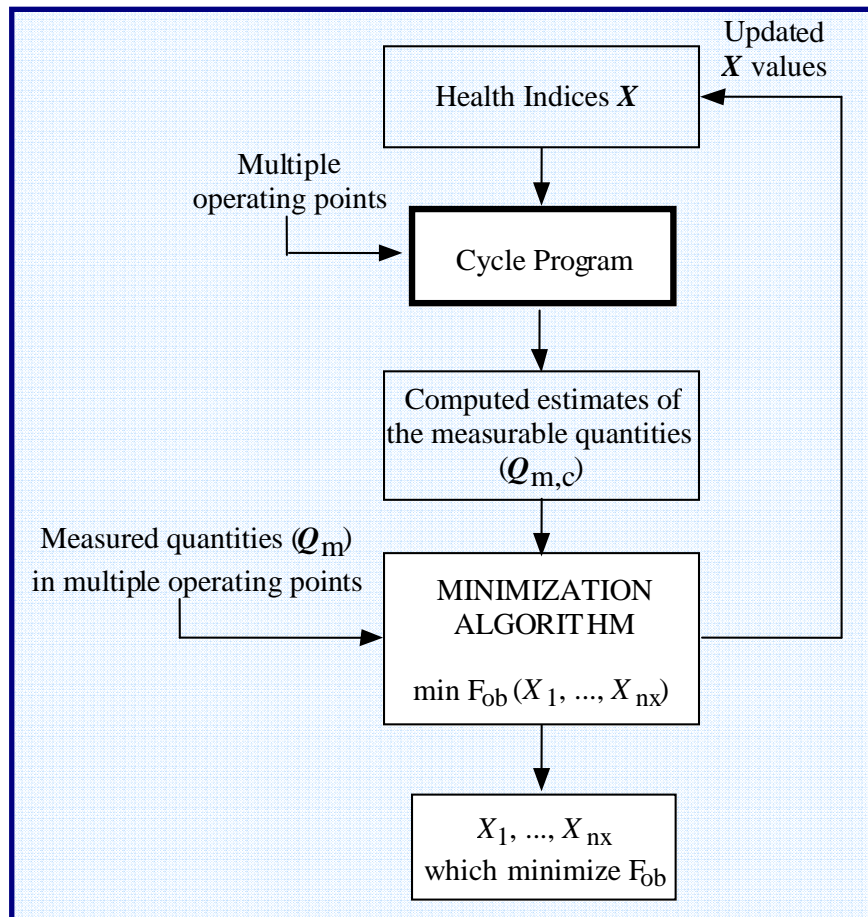
➤ k_B accounts for the scatter of the considered sample

➤ The left-hand side term of test criterion is updated at each step (off-line data processing!)

The diagnostic process (4/4)



Determination of GT Health Indices



GT Characteristic Parameters determination can be performed by

minimizing F_{ob}

(sum of the square differences between measured and computed values of the measurable variables, performed on one or multiple operating points)

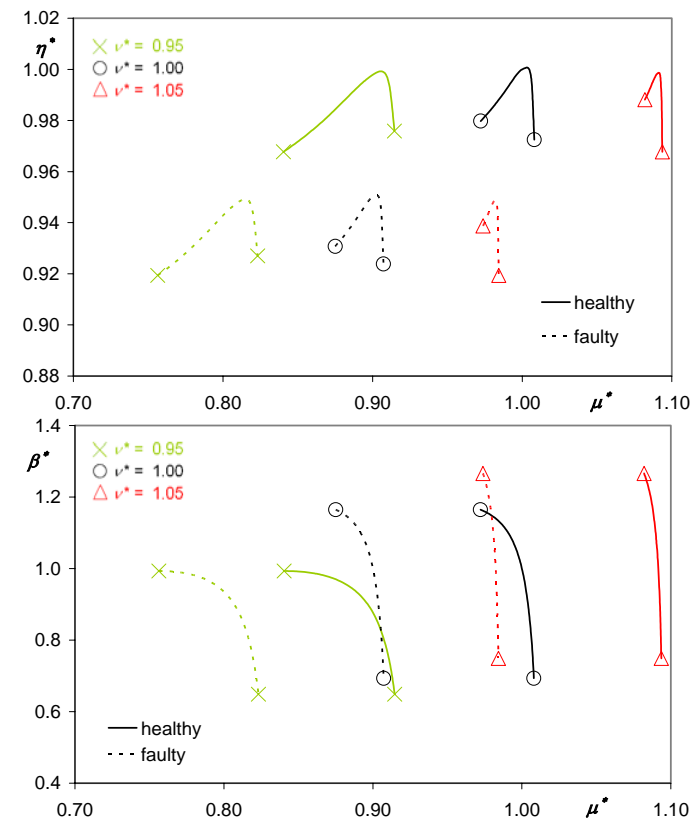
$$F_{ob}(X_1, \dots, X_{N_x}) = \frac{1}{N_{op}} \sum_{j=1}^{N_{op}} \left[\sum_{i=1}^{N_m} w_i \left(\frac{Q_{m,c} - Q_m}{Q_m} \right)_i^2 \right]_j$$

Parameters variations with respect to their expected values in “new and clean condition” (all parameters =1) determines GT Health State

Fault simulation

Gas turbine operating state determination consists of the assessment of the modification, due to deterioration and fault, of performance and geometric data characterizing machine components.

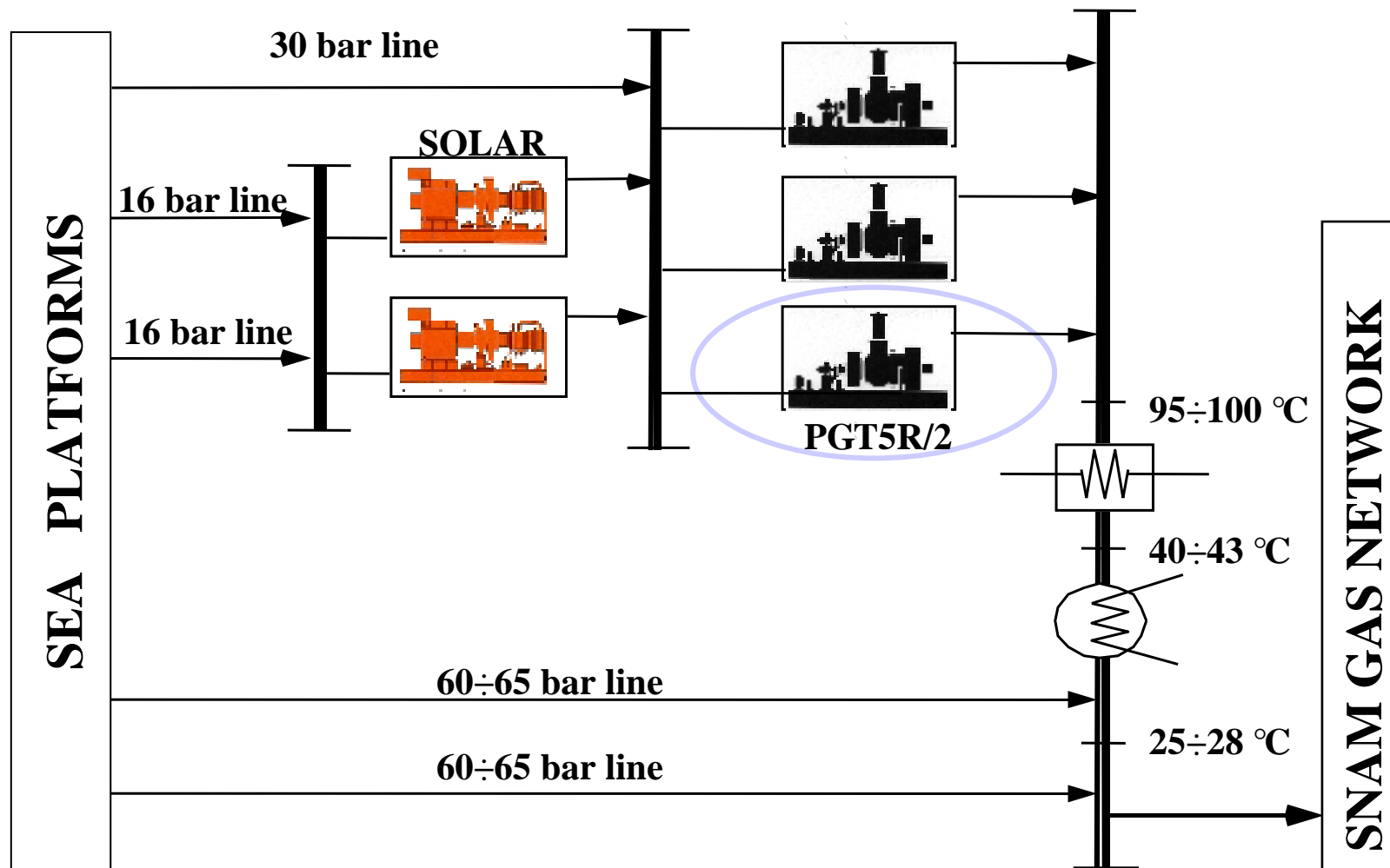
Effects are usually simulated by multiplying **point by point** the performance maps in new and clean condition by **scaling factors**.



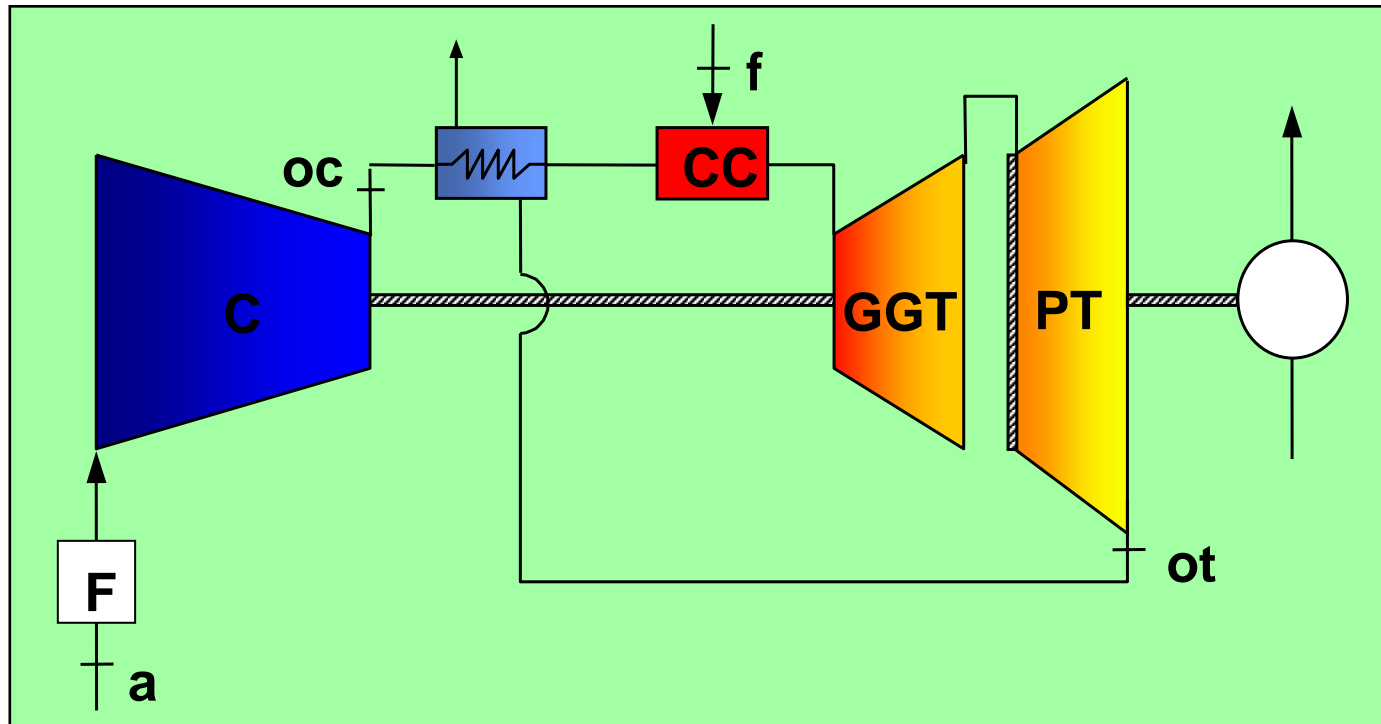
Remarks on multi-point analysis

- When poor instrumentation is available, only few parameters can be determined and with a not-very-high accuracy
- To overcome these problems, **Multiple Operating Point Analysis** can be used.
 - The method determines GT Health Indices by processing measurement sets taken in different working conditions
 - The method compensates for the lack of measured quantities with the measurements taken at different operating points
- By means of this method it is possible to:
 - calculate a **number of $X_v >$ number of Q_m**
 - improve accuracy
- In the following, the Multiple Operating Point Analysis will be applied **before** and **after** a **maintenance stop**

Application to a natural gas compression plant



Lay out of the 5.2 MW PGT5R/2 gas turbine



Six Q_{wp} meas. to define the working point: $N_{GGT}, N_{PT}, P_{PT}, p_a, T_a, RH_a$

Three Q_m meas. are available: p_{oc}, T_{oc}, T_{ot}

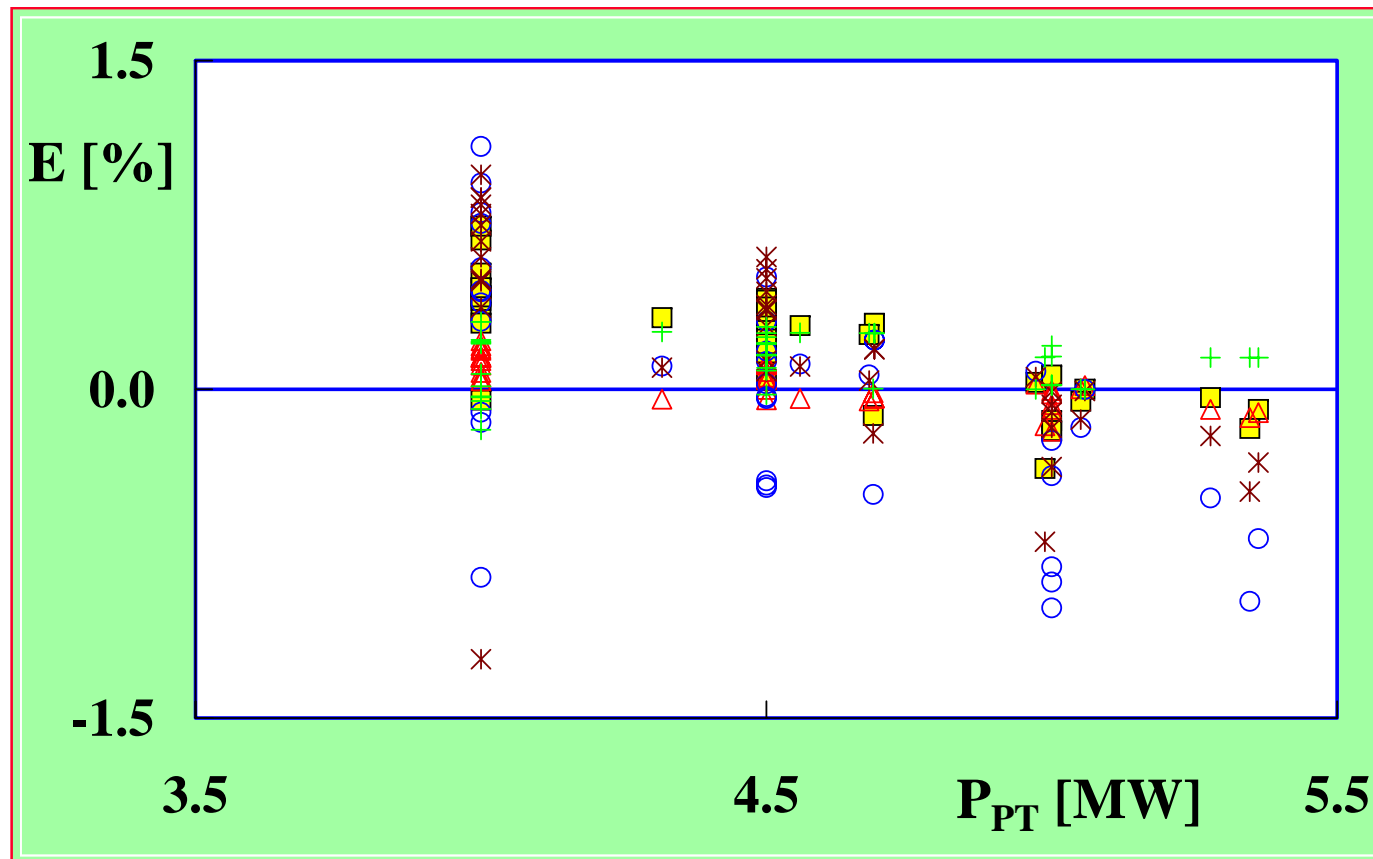
Three Health Indices can be determined: $\eta_C, \mu_C, \eta_{GGT}$

Lack of measurement

- Lack of fuel mass flow rate measurement (\dot{M}_f).
Only the total fuel mass flow feeding the three PGT5R/2 GTs is available
- Other measurements not available:
 - pressure and temperature between the gas generator and the power turbine (p_{GGT} , T_{GGT})
 - gas side and air side pressure drops of the recuperator (Δp_{air} , Δp_{gas})
 - air inlet mass flow rate (\dot{M}_a)

- The methodology was applied to a poorly instrumented plant, since it represents a selective test for the proposed diagnostic system
- Moreover, poor instrumented plants are highly widespread and, thus, the application to such cases seems particularly interesting

Cycle Program calibration

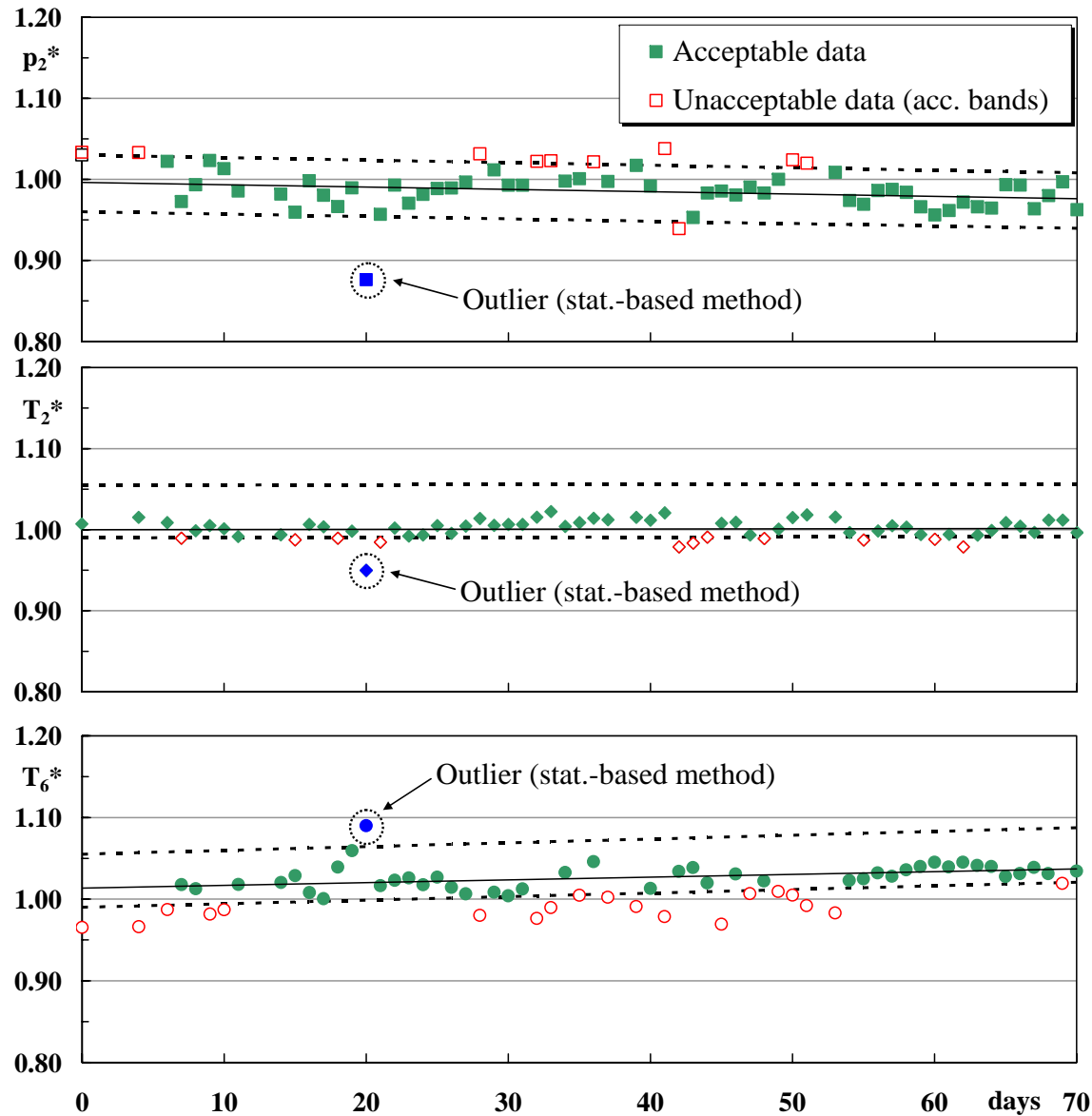


Errors between measured and computed value for

$$M_{\text{fuel}} - T_{\text{ot}} - M_{\text{air}} - T_{\text{oc}} - p_{\text{oc}}$$

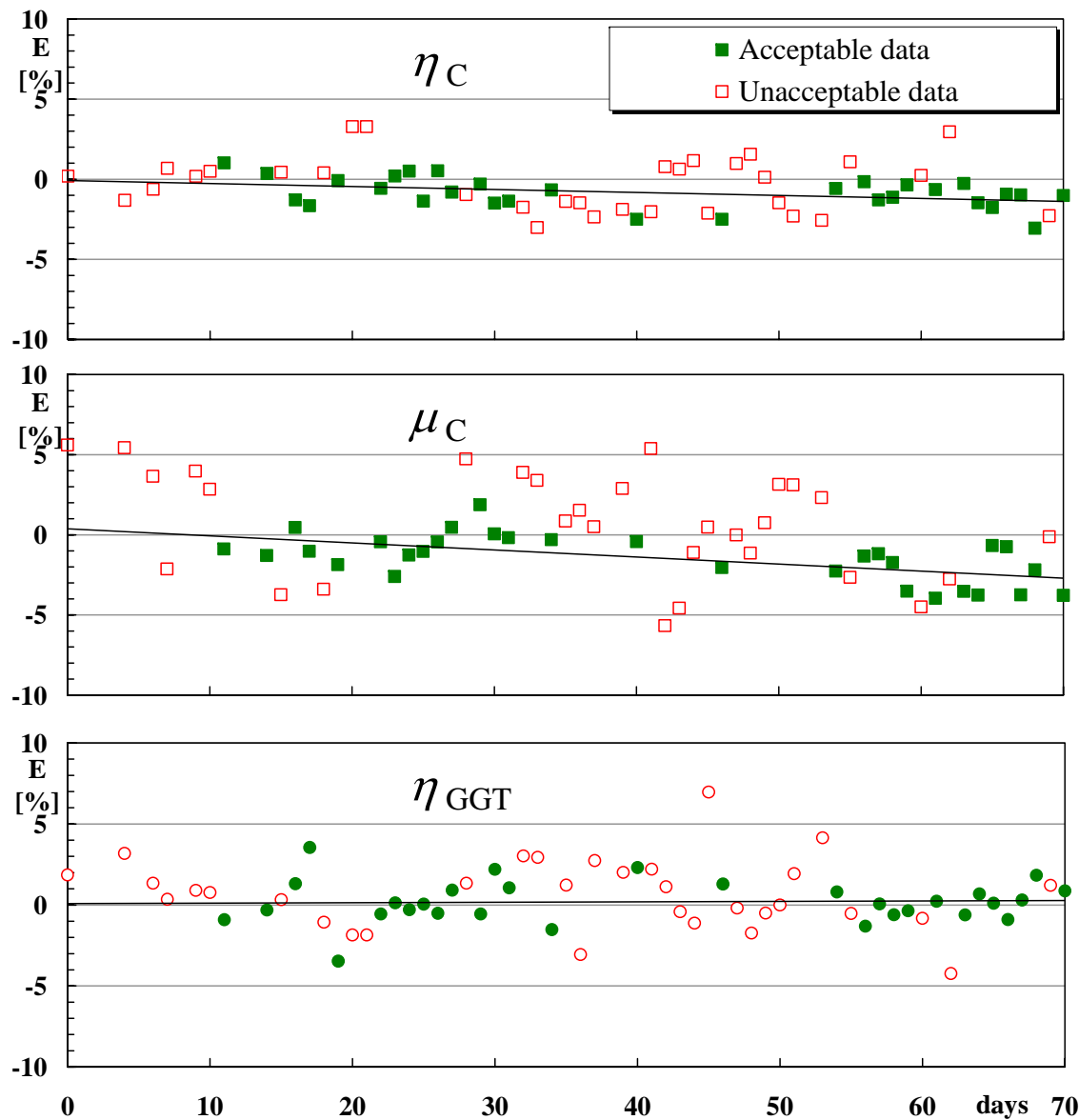
Six operating points (3.4 – 5.0 MW)

Normalized measurement trend analysis (Trend Analysis)



- Meas. scattering due to the uncertainties in field measurement readings
- The stat.-based method reveals that only one measurement set (day #20) is unacceptable. Thus, the stat.-based method is **less** restrictive than acceptability bands
- $p_{oc} \downarrow$ (2 % in 70 days)
and $T_{oc} \cong \Rightarrow$ comp. fouling
- T_{ot} slightly \uparrow

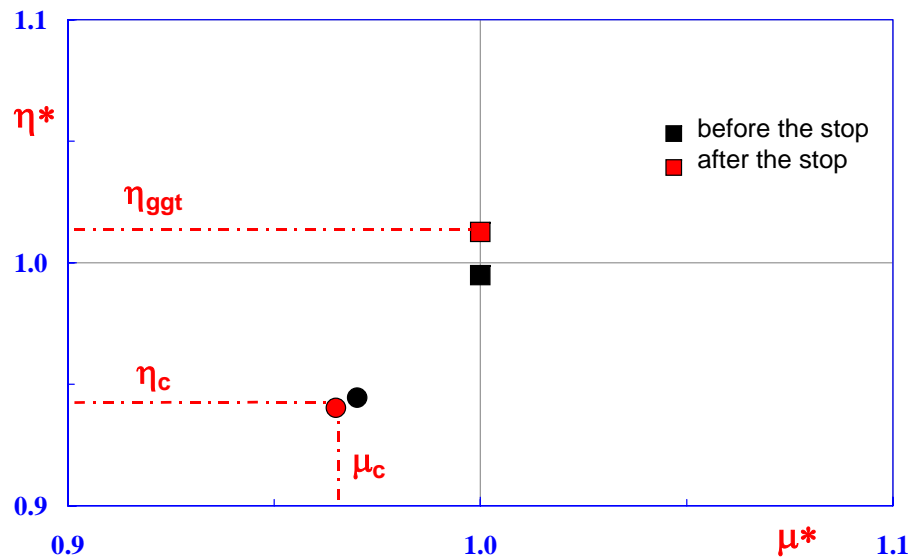
Health Indices estimation (single-point analysis)



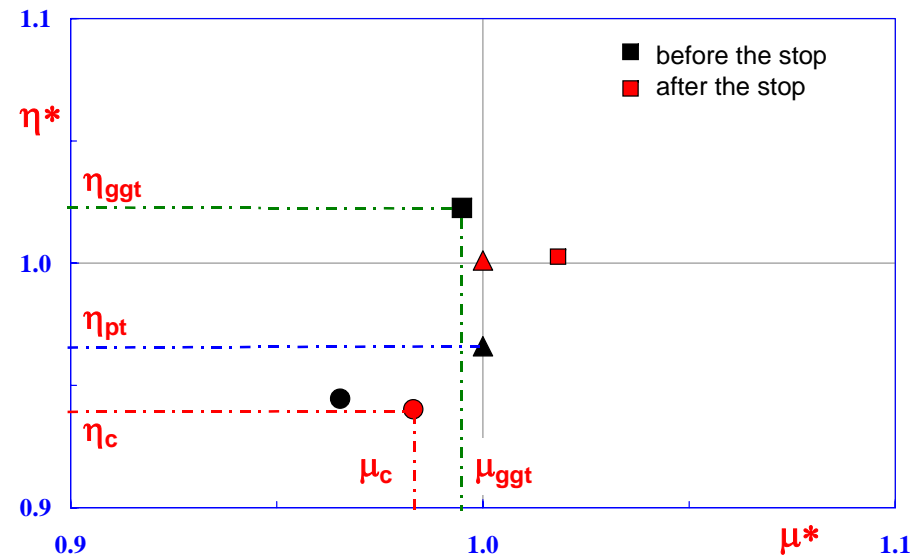
- Remarkable reduction of the scattering of HI trends, by using acceptable measurement sets only
- Over a period of 2 months, $\eta_C \downarrow$ (1.0 %) and $\mu_C \downarrow$ (2.5 %) \Rightarrow comp. fouling
- η_{GGT} almost constant \Rightarrow no significant health state change

Health Indices estimation (multi-point analysis)

Three parameters as problem variables η_c , μ_c , η_{ggt}



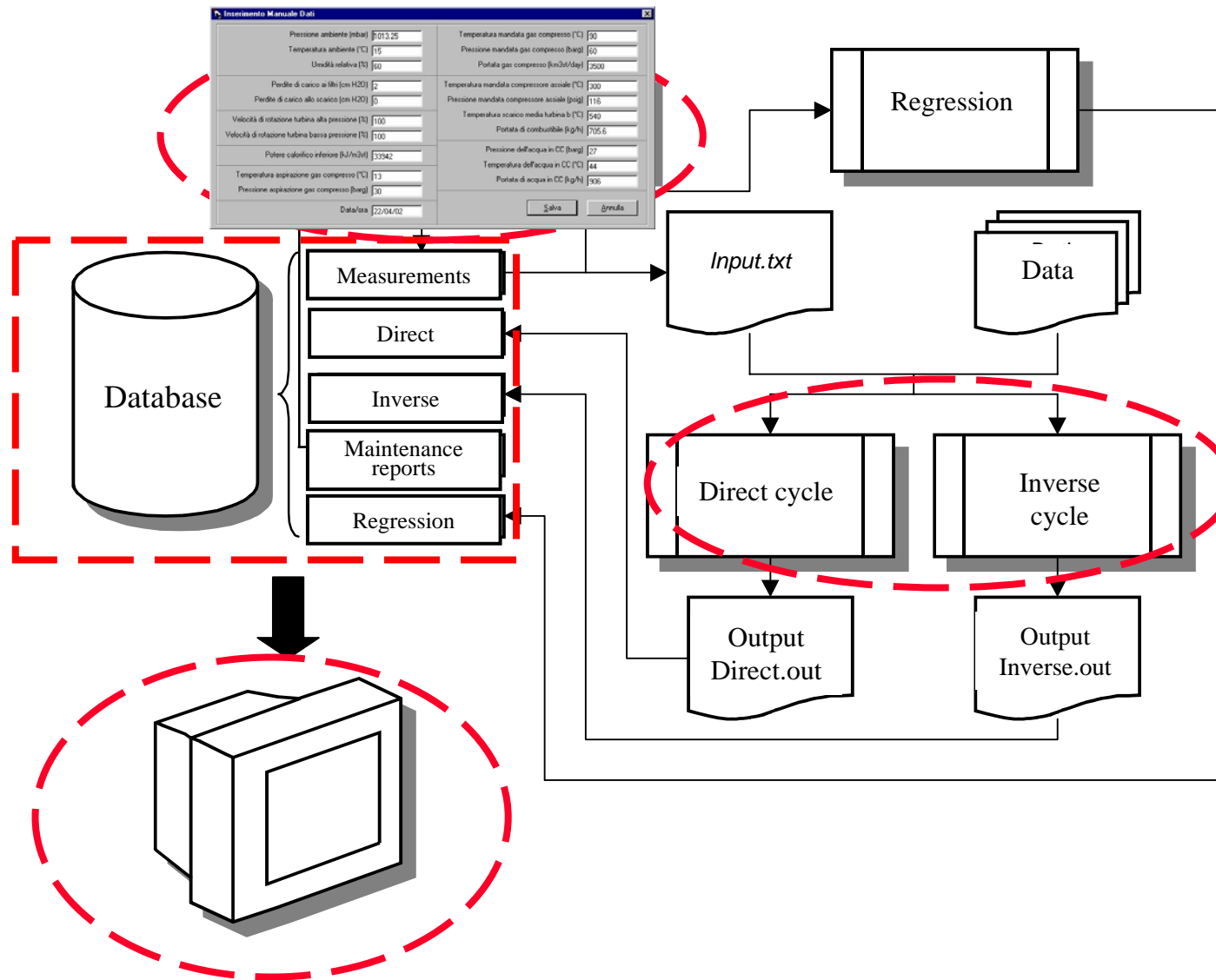
Five parameters as problem variables η_c , μ_c , η_{ggt} , μ_{ggt} , η_{pt}



More convincing results by using five HIs as problem variables:

- 3-His \Rightarrow no improvement due to maintenance
- 5-His \Rightarrow increase in the corrected mass flows (both C and GGT)

Health Monitoring System for the Compression Plant

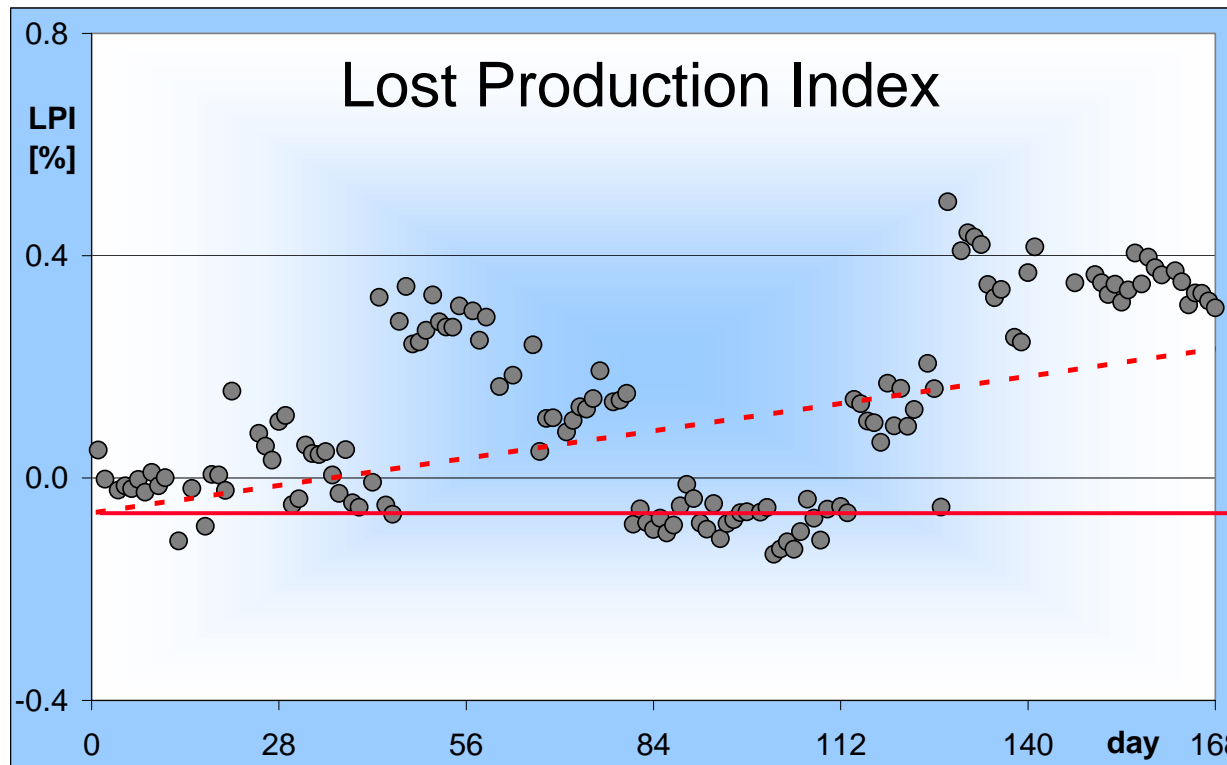


Lost production index

$$\text{LPI} = \frac{Q_{\text{gasC}} - Q_{\text{gasM}}}{Q_{\text{gasC}}}$$

C = clean condition - M = measured

- LPI increase = decrease of actual production
- LPI quantifies (also economically) gas turbine loss of performance



**The compressed
gas production
loss is**

+ 13 %

Conclusions

The methodology proved effective in supporting plant operation and maintenance management:

- Identification of unreliable measurements sets and remarkable reduction of the scattering of the measurement trends
- Gas turbine health state determination over a 2-month period: compressor fouling, while gas generator turbine was not suffering from significant changes in health state
- The multi-point analysis (applied before and after a maintenance stop) allowed a more detailed analysis
- Software to automate the diagnostic process and to support plant operation and management: the loss of production, due to gas turbine deterioration, was identified