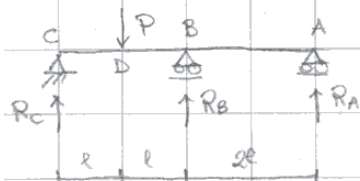


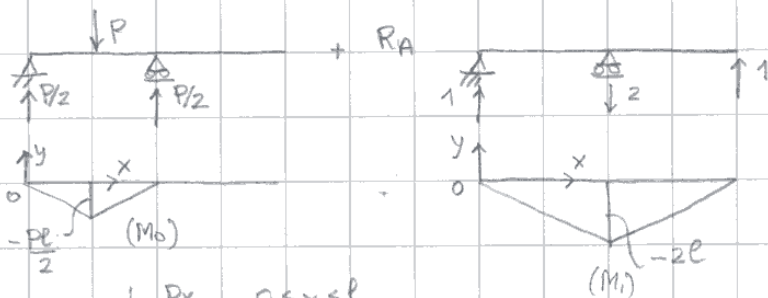
EXERCISE 1



The structure is statically indeterminate, i.e. equilibrium eqns are not sufficient to determine the reactions:

$$(\#1) \begin{cases} R_A + R_B + R_C = P & \text{Two eqns} \\ R_B 2l + R_A 4l = P l & \text{but three unknowns!} \end{cases}$$

To calculate the reaction, we adopt the following strategy
We apply the principle of superposition:



$$M_0(x) = \begin{cases} -\frac{Px}{2}, & 0 \leq x \leq l \\ \frac{P}{2}(x-2l), & l \leq x \leq 2l \\ 0, & 2l \leq x \leq 4l \end{cases}$$

$$M_1(x) = \begin{cases} -x, & 0 \leq x \leq 2l \\ (x-4l), & 2l \leq x \leq 4l \end{cases}$$

By superposition: $M(x) = M_0(x) + R_A M_1(x)$

The deformation energy takes the form:

$$E_d = \frac{1}{2EI} \int_0^{4l} M^2(x) dx = \frac{1}{2EI} \int_0^{4l} (M_0(x) + R_A M_1(x))^2 dx \quad (\#2)$$

On new of Maupertuis's thm, R_A is the solution to the equation:

$$0 = \frac{\partial E_d}{\partial R_A} = \frac{1}{EI} \int_0^{4l} M_1(x) (M_0(x) + R_A M_1(x)) dx$$

or equivalently,

$$\left(\int_0^{4l} M_0(x) M_1(x) dx \right) + R_A \left(\int_0^{4l} M_1^2(x) dx \right) = 0$$

$$R_A = - \frac{\left(\int_0^{4l} M_0(x) M_1(x) dx \right)}{\left(\int_0^{4l} M_1^2(x) dx \right)} \quad (\#3)$$

We now calculate the two terms:

$$\int_0^{4l} M_0(x) M_1(x) dx = \int_0^l \frac{P}{2} x^2 dx + \int_l^{2l} \frac{P}{2} (2lx - x^2) dx$$

$$= \frac{Pe^3}{6} + \frac{P}{2} \left[lx^2 - \frac{x^3}{3} \right]_l^{2l} = \frac{Pe^3}{6} + \frac{Pe^3}{2} \left(4 - \frac{8}{3} - 1 + \frac{1}{3} \right)$$

$$= Pe^3 \left(\frac{1}{6} + \frac{3}{2} - \frac{1}{6} \right) = Pe^3 \left(\frac{3}{2} - 1 \right) = \frac{Pe^3}{2}$$

$$\int_0^{4l} M_1^2(x) dx = 2 \int_0^{2l} x^2 dx = \frac{2}{3} \cdot 8l^3 = \frac{16l^3}{3}$$

by symmetry

After substituting into (#3), we obtain: $R_A = -\frac{Pe^3}{2} \cdot \frac{3}{16l^3} = -\frac{3}{32} P$ (#4)

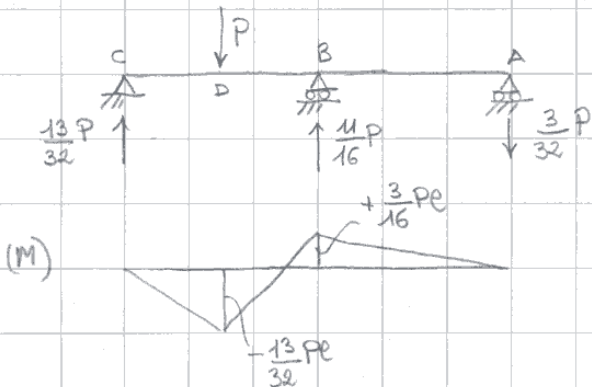
this sign here means that R_A is pointing downwards!

To calculate R_B and R_C , we substitute relation (#4) into (#1):

$$\begin{cases} -\frac{3}{32} P + R_B + R_C = P \\ 2R_B - 4 \cdot \frac{3}{32} P = P \end{cases} \rightarrow R_B = \frac{1}{2} \left(\frac{3}{8} + 1 \right) P = \frac{11}{16} P$$

$$\rightarrow R_C = P + \frac{3}{32} P - \frac{11}{16} P = \frac{(32+3-22)}{32} P = \frac{13}{32} P$$

At equilibrium, the reactions and the bending moment are as depicted in the fig.



$$M(x) = \begin{cases} -\frac{13}{32} Px, & 0 \leq x \leq l, \\ +\frac{19}{32} P \left(x - \frac{32}{19} l \right), & l \leq x \leq 2l, \\ -\frac{3}{32} P(x-4l), & 2l \leq x \leq 4l. \end{cases} \quad \text{(#5)}$$

To calculate the vertical displacement of the point D, let us still consider the deformation energy given by eqn (#2).

In view of Castigliano's theorem, we have:

$$U_0 = \frac{\partial E_d}{\partial P} = \frac{1}{EI} \int_0^{4l} x(M_0 + RA M_1) \left(\frac{\partial M_0}{\partial P} + RA \frac{\partial M_1}{\partial P} + \frac{\partial RA}{\partial P} M_1 \right) dx$$

this term vanishes because M_1 is independent of P

$$= \left(\frac{1}{EI} \int_0^{4l} \underbrace{(M_0 + RA M_1)}_M \frac{\partial M_0}{\partial P} dx \right) + \frac{\partial RA}{\partial P} \left(\frac{1}{EI} \int_0^{4l} (M_0 + RA M_1) M_1 dx \right)$$

this term vanishes because of (#3).

Thus, we obtain:

$$U_0 = \frac{1}{EI} \int_0^{4l} M(x) \frac{\partial M_0(x)}{\partial P} dx$$

$$\frac{\partial M_0(x)}{\partial P} = \begin{cases} -\frac{x}{2}, & 0 \leq x \leq l \\ \frac{1}{2}(x-2l), & l \leq x \leq 2l \\ 0, & 2l \leq x \leq 4l \end{cases}$$

$$= \frac{1}{EI} \left(\int_0^l \left(-\frac{13P}{32} x \right) \left(-\frac{x}{2} \right) dx + \int_l^{2l} \left(\frac{19P}{32} x - Pl \right) \frac{1}{2}(x-2l) dx \right)$$

$x' = 2l - x$
 $\hookrightarrow x = 2l - x'$

$$= \frac{13P}{64EI} \int_0^l x^2 dx + \frac{1}{EI} \int_l^{2l} \left[\frac{19P}{32} (2l - x') - Pl \right] \frac{1}{2} (-x') (-dx')$$

$$= \frac{13P}{64EI} \int_0^l x^2 dx - \frac{1}{2EI} \int_0^l \left(\frac{19Pl}{16} - Pl - \frac{19P}{32} x' \right) x' dx'$$

$$= \frac{13P}{64EI} \frac{l^3}{3} - \frac{1}{2EI} \int_0^l \left[\frac{3Pl}{16} x' - \frac{19P}{32} (x')^2 \right] dx'$$

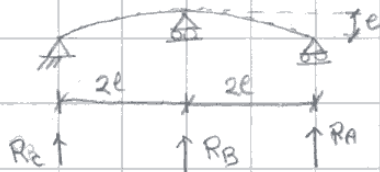
$$= \frac{13Pl^3}{192EI} - \frac{1}{2EI} \left[\frac{3Pl}{16} \frac{(x')^2}{2} - \frac{19P}{32} \frac{(x')^3}{3} \right]_0^l$$

$$= \frac{13}{192} \frac{Pl^3}{EI} + \frac{5}{96} \frac{Pl^3}{EI} = \frac{23}{192} \frac{Pl^3}{EI}$$

EXERCISE 2.



Initial undeformed and stress-free configuration

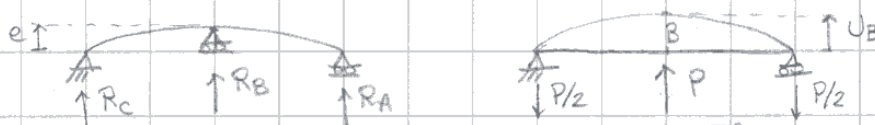


Deformed and stress configuration after defect
(for symmetry reasons, we expect $R_A = R_C$!)

Again, equilibrium eqns are not sufficient to determine the reactions:

$$(\#7) \begin{cases} R_A + R_B + R_C = 0 \\ R_B 2l + R_A 4l = 0 \end{cases} \quad \begin{array}{l} \text{Two eqns but} \\ \text{three unknowns!} \end{array}$$

This time, to calculate the reactions, it is convenient to use Betti's thm:



$$P e = R_B U_B \quad (\#7)$$

$$M(x) = \begin{cases} \frac{P}{2} x, & 0 \leq x \leq 2l \\ -\frac{P}{2} (x - 4l), & 2l \leq x \leq 4l \end{cases}$$

We now calculate U_B using Menabrea's thm:

$$E_d = \frac{1}{2EI} \int_0^{4l} M^2(x) dx$$

$$\begin{aligned} \hookrightarrow U_B &= \frac{\partial E_d}{\partial P} = \frac{1}{EI} \int_0^{4l} M(x) \frac{\partial M(x)}{\partial P} dx = \frac{1}{EI} \int_0^{2l} \left(\frac{P}{2} x \right) \left(\frac{x}{2} \right) dx \\ &= \frac{P}{2EI} \int_0^{2l} x^2 dx = \frac{P}{2EI} \left(\frac{8l^3}{3} \right) = \frac{4}{3} \frac{Pl^3}{EI} \end{aligned} \quad (\#8)$$

Substituting (#8) into (#7) gives:

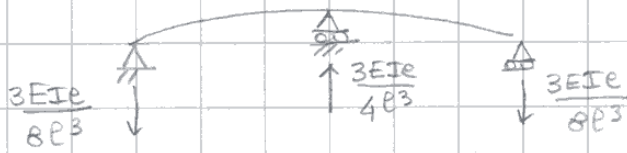
$$R_B = \frac{P e}{U_B} = \frac{3EI P e}{4Pl^3} = \frac{3EIE}{4l^3} \quad (\#9)$$

We calculate the remaining reactions by substituting (#9) into (#7):

$$R_A = -\frac{R_B}{2} = -\frac{3EI\epsilon}{8l^3}$$

$$R_C = -R_A - R_B = -\frac{3EI\epsilon}{4l^3} + \frac{3EI\epsilon}{8l^3} = -\frac{3EI\epsilon}{8l^3}$$

The reactions are as depicted in the following figure.



And the bending moment can be calculated as follows:

