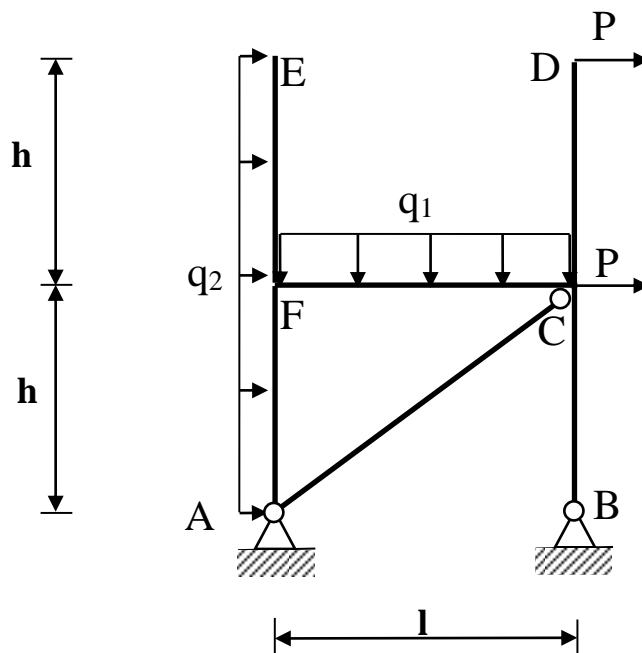


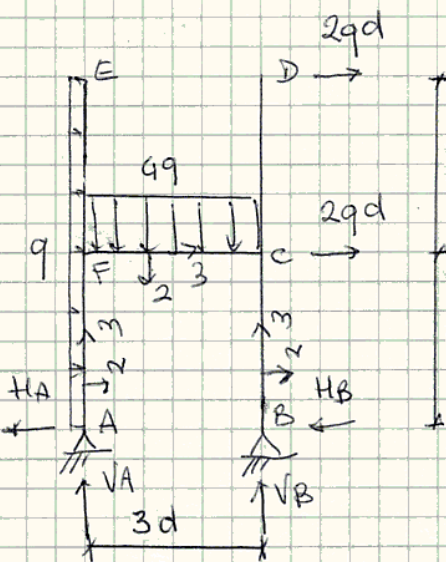
**CORSO DI LAUREA IN INGEGNERIA MECCANICA**  
**UNIVERSITÀ DI FERRARA**  
**PROVA SCRITTA DI STATICA**  
**13/01/2016**



$$l = 3 \text{ m}, h = 4 \text{ m}$$
$$q_1 = 20 \text{ kN/m}, q_2 = 5 \text{ kN/m}, P = 10 \text{ kN},$$
$$E = 210 \text{ GPa}, \sigma_{\text{amm}} = 240 \text{ MPa}$$

La travatura in figura deve essere realizzata con profilati IPE.

- Disegnare i diagrammi quotati delle caratteristiche della sollecitazione in assenza del controvento  $AC$ .
- Dimensionare la travatura.
- Calcolare lo spostamento orizzontale del nodo  $C$ .
- Disegnare i diagrammi quotati delle caratteristiche della sollecitazione anche in presenza del controvento  $AC$ .

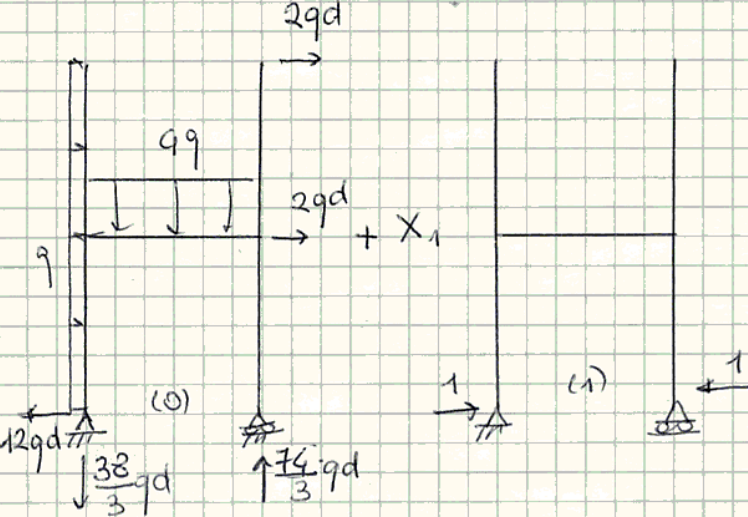


$q = 5 \text{ kN/m}$   
 $d = 1 \text{ m}$

$$\begin{cases}
 H_A + H_B = 12qd \\
 V_A + V_B = 12qd \\
 (A) \quad V_B \cdot 3d = 3 \cdot q \cdot \frac{3}{2} d^2 + 2qd \cdot 4d + 2qd \cdot 8d + 8qd \cdot 4d \\
 \quad \quad \quad = qd^2 (18 + 8 + 16 + 32) = 74qd^2
 \end{cases}$$

$$\begin{cases}
 V_B = 74/3 \text{ } qd = 123,3 \text{ kN} \\
 V_A = (12 - 74/3) qd = -\frac{38}{3} qd = -63,3 \text{ kN} \\
 H_A + H_B = 12qd
 \end{cases}$$

La trave è 1 volta iperstatica. Il supporto iperstatico:  $X_1 = H_B$

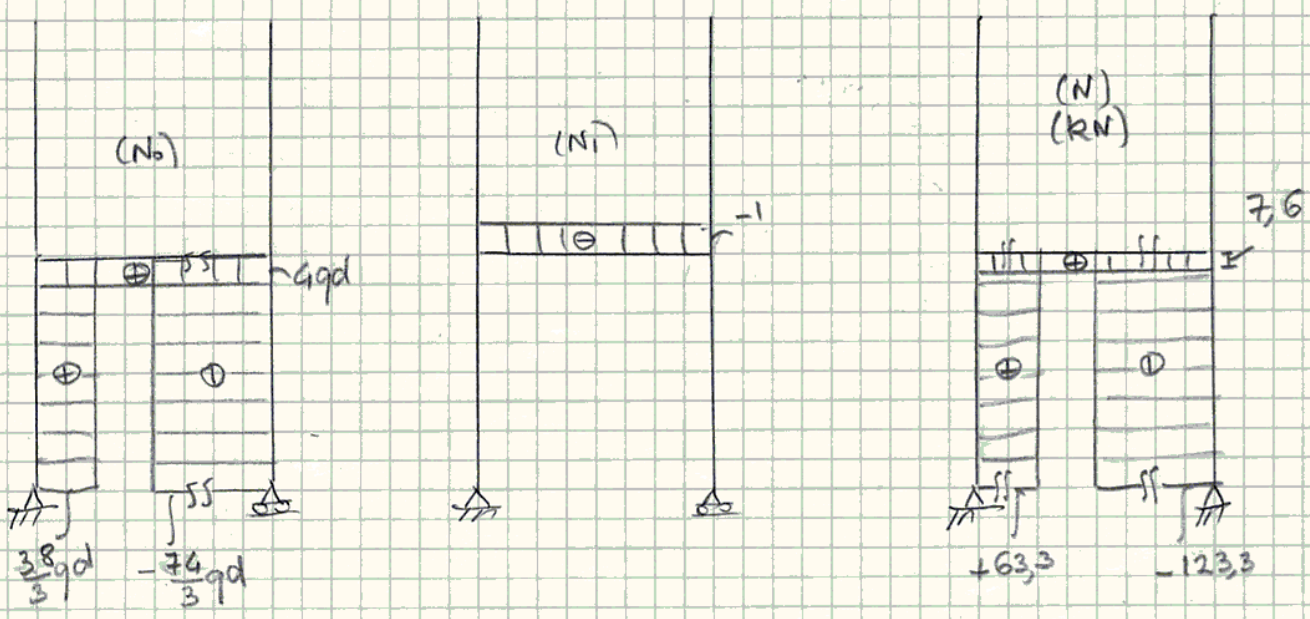
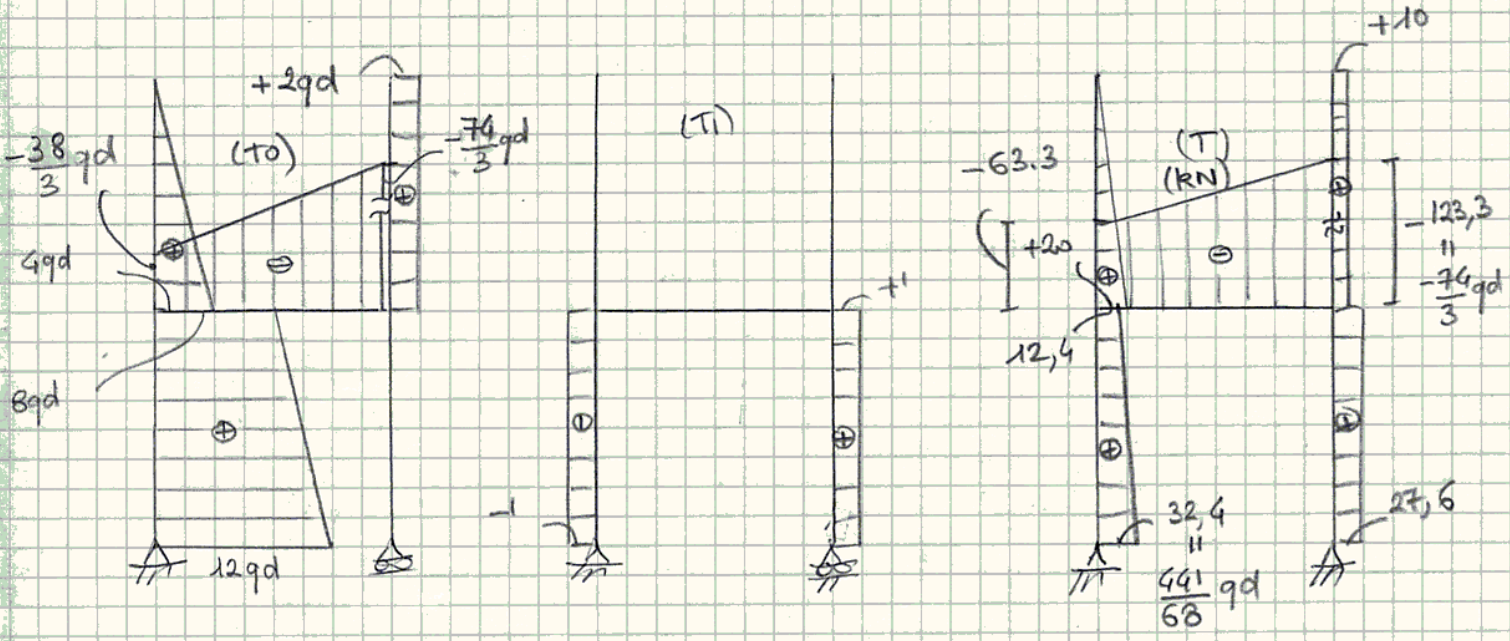
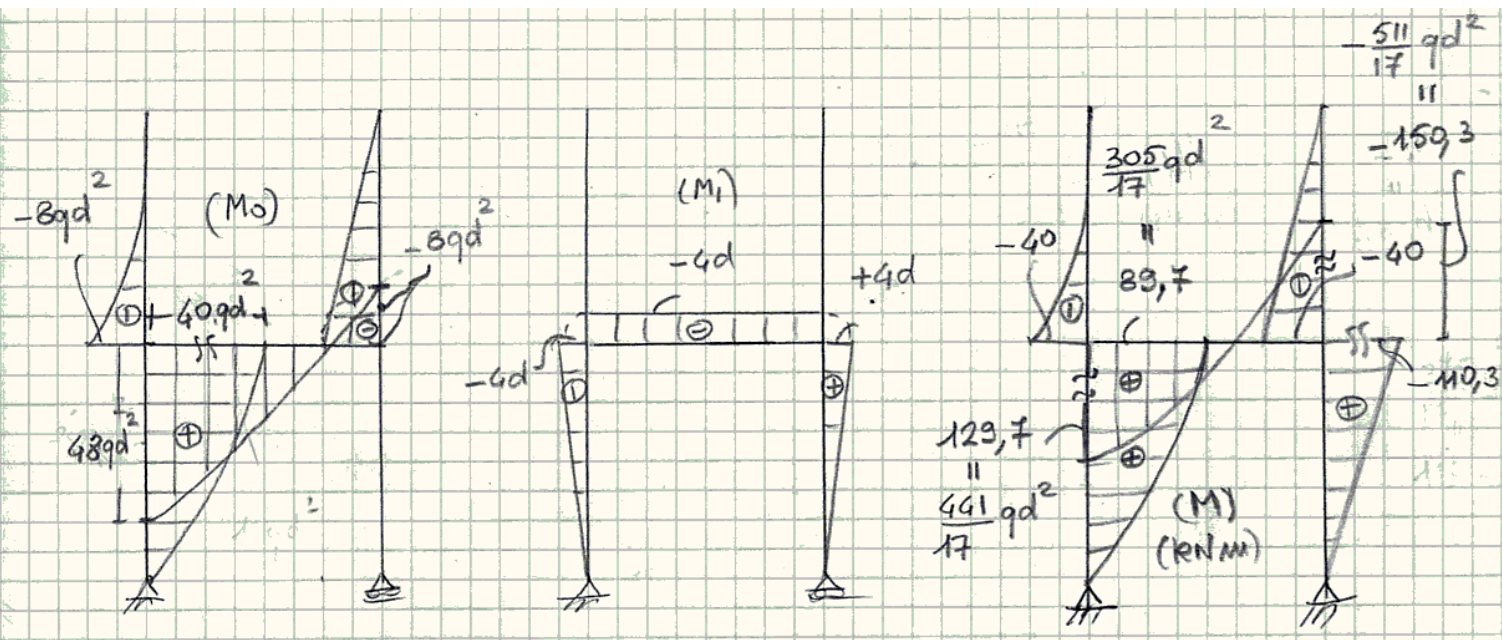


$$EI_1 M_{10} = \int_0^{4d} (-x) \left( -\frac{qx^2}{2} + 12qdx \right) dx + \int_0^{3d} (-4d) \left( -\frac{4qx^2}{2} - \frac{38}{3} qdx + 48qd^2 \right) dx$$

$$= -224qd^4 - 276qd^4 = -500qd^4$$

$$EI_1 \gamma_{11} = 2 \cdot \frac{1}{3} \cdot 4d \cdot 16d^2 + 3d \cdot 16d^2 = 16d^3 \left( 3 + \frac{8}{3} \right) = \frac{272}{3} d^3$$

$$X_1 = \frac{3 \cdot 500}{272} qd = \frac{375}{68} qd = 27,57 \text{ kN}$$



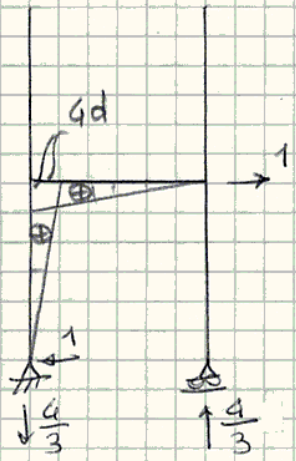
Dimensionamento:

$$W_1 \geq \frac{M_{max}}{\sigma_{AMM}} = \frac{150,3 \cdot 10^3}{240} \cdot 10^6 \text{ cm}^3 = \frac{15030}{24} \text{ cm}^3 = 626,25 \text{ cm}^3$$

↳ IPE 330

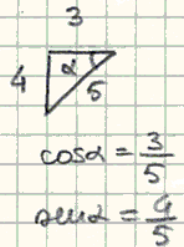
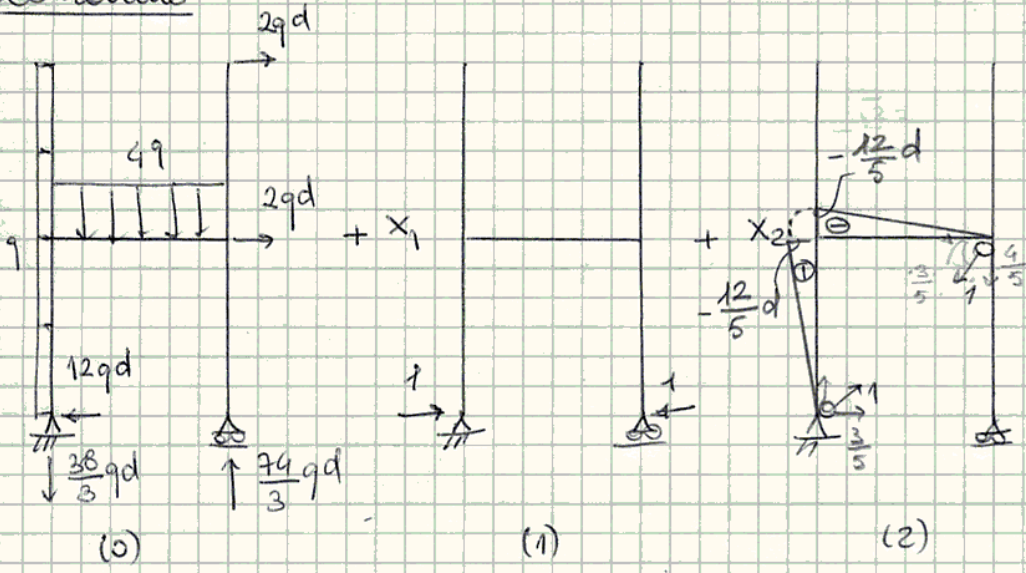
$$\begin{cases} W_1 = 713,1 \text{ cm}^3 \\ I_1 = 11770 \text{ cm}^4 \\ A = 62,61 \text{ cm}^2 \end{cases}$$

Spostamento orizzontale in C:



$$\begin{aligned} 1. \Delta_C &= \frac{1}{EI_1} \left[ \int_0^{4d} (x) \left( -qx \frac{x^2}{2} + \frac{4q}{68} qdx \right) dx + \int_0^{3d} \left( \frac{4}{3}x \right) \left( -4qx \frac{x^2}{2} + \frac{74}{3} qdx \right) dx \right] \\ &= \frac{1608}{17} \frac{qd^4}{EI} + \frac{1048}{17} \frac{qd^4}{EI} = \frac{2856}{17} \frac{qd^4}{EI} = 168 \frac{qd^4}{EI} \\ &= \frac{168 \cdot 5,0 \cdot 10^3}{210 \cdot 11770} \cdot 10^2 \text{ cm} \\ &= \frac{168 \cdot 500}{21 \cdot 1177} \text{ cm} = 3,4 \text{ cm} \end{aligned}$$

Caricovento



$$EI_1 \eta_{10} = -500 qd^4$$

$$\begin{aligned} EI_1 \eta_{20} &= \int_0^{4d} \left( \frac{3}{5}x \right) \left( -qx \frac{x^2}{2} + 12qdx \right) dx + \int_0^{3d} \left( -\frac{4}{5}x \right) \left( -4qx \frac{x^2}{2} + \frac{74}{3} qdx - 8qd^2 \right) dx \\ &= -\frac{672}{5} qd^4 - \frac{582}{5} qd^4 = -\frac{1254}{5} qd^4 \end{aligned}$$

$$EI_1 \eta_{11} = \frac{272}{3} d^3 ; EI_1 \eta_{12} = \frac{1}{3} 4d \cdot 4d \cdot \frac{12}{5} d + (+4d) 3d \frac{1}{8} \frac{12}{5} d = \frac{136}{5} d^3$$

$$EI_1 \gamma_{22} = \frac{1}{3} qd \cdot \frac{144}{25} d^2 + \frac{1}{8} qd \cdot \frac{144}{25} d^2$$

$$= \frac{7}{3} \cdot \frac{144}{25} d^3 = \frac{336}{25} d^3$$

$$\begin{bmatrix} \frac{272}{3} & \frac{136}{5} \\ \frac{136}{5} & \frac{336}{25} \end{bmatrix} \begin{bmatrix} X_1 \\ X_2 \end{bmatrix} = qd \begin{bmatrix} 500 \\ \frac{1254}{5} \end{bmatrix}$$

$$\begin{cases} X_1 = -\frac{159}{748} qd = -1,06 \text{ kN} \\ X_2 = \frac{210}{11} qd = 95,45 \text{ kN} \end{cases}$$

Poiché  $X_1 \approx 1\%$  di  $X_2$ , si ha che il tratto BC è praticamente ridotto a flessione, essendo il taglio nullo ovunque sul tratto BC ed assorbito dal controvento AC. I diagrammi finali si possono quindi ottenere con buona approssimazione mediante sovrapposizione dei sistemi (0) e (2).